

Mapping between s-plane & z-plane:-

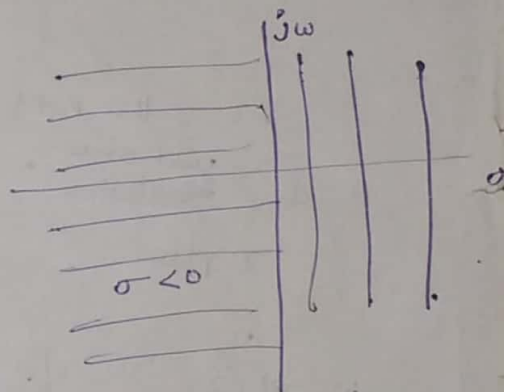
→ Since the complex variables z and s are related by $z = e^{Ts}$, the pole and zero locations in the z -plane are related to the pole and zero locations in the s -plane.

let $s = \sigma + j\omega$.

then $z = e^{Ts} = e^{T\sigma} e^{jT\omega}$
 $= e^{T\sigma} e^{j(T\omega + 2\pi k)}$

i.e. There are infinitely many values of s for each value of z .

→ s-plane $s = \sigma + j\omega$.



if σ is negative → left half s-plane

if σ is 0 → $j\omega$ axis.

if σ is positive → Right half side

→ $z = e^{Ts} = e^{T\sigma} e^{j(T\omega + 2\pi k)}$

$|z| = e^{T\sigma}$; $\angle z = \omega T$

let $z = u + jv$
 $|z| = u^2 + v^2$

if $\sigma < 0$ (left half s-plane) → $|z| < 1$

from (i) ⇒ if $\sigma = 0$ ($j\omega$ axis) ⇒ $|z| = 1$ ← eqn of circle.

i.e. $j\omega$ axis in s -plane maps to unit circle in z -plane

if $\sigma < 0$ (L.H.S) $|z| = e^{-T\sigma} < 1$.

i.e circle whose radius is less than 1 or interior of unit circle.

if $\sigma > 0$ $|z| = e^{T\sigma} > 1$ outside of unit circle.

$\Rightarrow \rightarrow$ angle of z $\angle z = \omega T$

let $\omega_s =$ sampling frequency $= \frac{2\pi}{T}$.

\therefore angle varies from $-\infty$ to ∞ as ω varies from ∞ to $-\infty$.

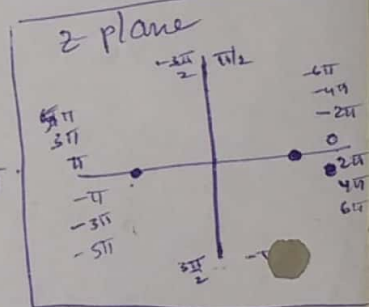
① if a point moves from $-j\frac{1}{2}\omega_s$ to $j\frac{1}{2}\omega_s$ in s-plane.

then if $\omega = \frac{1}{2}\omega_s \Rightarrow \angle z = \frac{1}{2} \cdot \frac{2\pi}{T} \cdot T = \pi$

if $\omega = -\frac{1}{2}\omega_s \Rightarrow \angle z = -\frac{1}{2} \cdot \frac{2\pi}{T} \cdot T = -\pi$

i.e the point from $-j\frac{1}{2}\omega_s$ to $j\frac{1}{2}\omega_s$ in s-plane maps to a ~~unit circle~~ semicircle starting from $-\pi$ to π in C.C.W direction in z-plane.

$\Rightarrow \Rightarrow$ ② if $\omega = \frac{1}{2}\omega_s \Rightarrow \angle z = \pi$
 $\omega = \frac{3}{2}\omega_s \Rightarrow \angle z = 3\pi$



i.e a point on $j\omega$ axis axis of s-plane which starts from $j\frac{1}{2}\omega_s$ to $j\frac{3}{2}\omega_s$ will map to a unit circle in the z-plane in C.C.W direction.

~~each strip~~ \rightarrow $j\omega$ axis in the s-plane \rightarrow ~~interior~~ unit circle in z-plane
 each strip of width ω_s in L.H.S \rightarrow maps to a unit circle.

→ The impact of sampling on a continuous signal is reflected defining of primary strip and complementary strip.

frequency boundaries of primary strip $\pm \frac{\omega_s}{2}$

frequency boundaries of complementary strips = multiples of $\frac{\omega_s}{2}$.

This phenomenon is caused by the periodic nature of z as a function of $s = \sigma + j\omega$.

$$z = e^{Ts} = e^{T(\sigma + j\omega)} = e^{T(\sigma + j\omega \pm \frac{2\pi k}{T})}$$

where $\omega_s \rightarrow$ sampling frequency

$T \rightarrow$ sampling time

$k = 0, 1, 2, \dots$

i.e. poles and zeros of the s -plane T transform function outside the primary strip are folded into the primary strip, possibly causing undesired performance.

→ The folded poles and zeros act as if they were originally in the primary strip, thus changing the system performance.

→ The s -plane poles $s = j\omega$ and $s = -j\omega$ in the primary strip are mapped to the z -plane poles $z = e^{j\omega T}$ & $z = e^{-j\omega T}$.

But these z -plane poles are also maps of s -plane poles

$$s = j\omega + \frac{2\pi k}{T}, j\omega + \frac{4\pi k}{T}, j\omega + \frac{6\pi k}{T} \dots \dots \dots \left. \vphantom{s} \right\}$$

$$s = \pm j\omega + \frac{2\pi k}{T}, \pm j\omega + \frac{4\pi k}{T}, \pm j\omega + \frac{6\pi k}{T} \dots \dots \dots \left. \vphantom{s} \right\} \text{ in the}$$

complementary strip. This means there are infinitely many values of s for each z .

→ Thus the largest frequency we can distinguish is

$$\omega = \frac{\omega_s}{2} \text{ (or) } \frac{\omega_s}{2}, \text{ which is half of the sampling frequency.}$$

→ Consider a representative point on $j\omega$ axis in s -plane.

As this point moves from $j\frac{1}{2}\omega_s$ to $j\frac{1}{2}\omega_s$

$\angle Z \rightarrow$ varies $-\pi$ to π in c.w.

As this point moves from $j\frac{1}{2}\omega_s$ to $j\frac{3}{2}\omega_s$.

the corresponding point traces out the unit circle once in the counter clockwise direction.

→ Thus as the point moves from $-\infty$ to ∞ on $j\omega$ axis, we trace the unit circle in the z -plane an infinite no. of times.

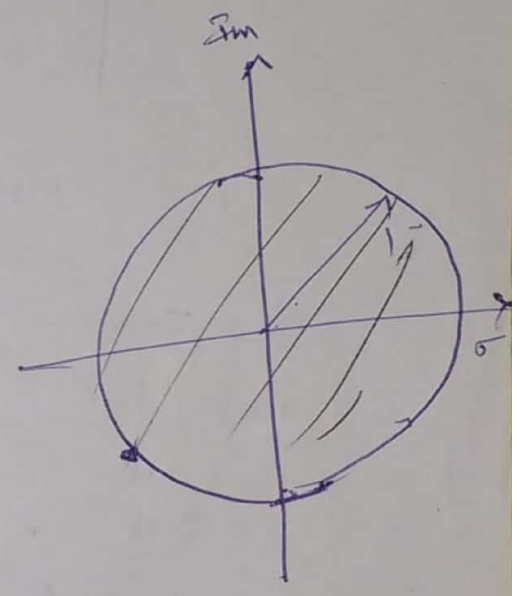
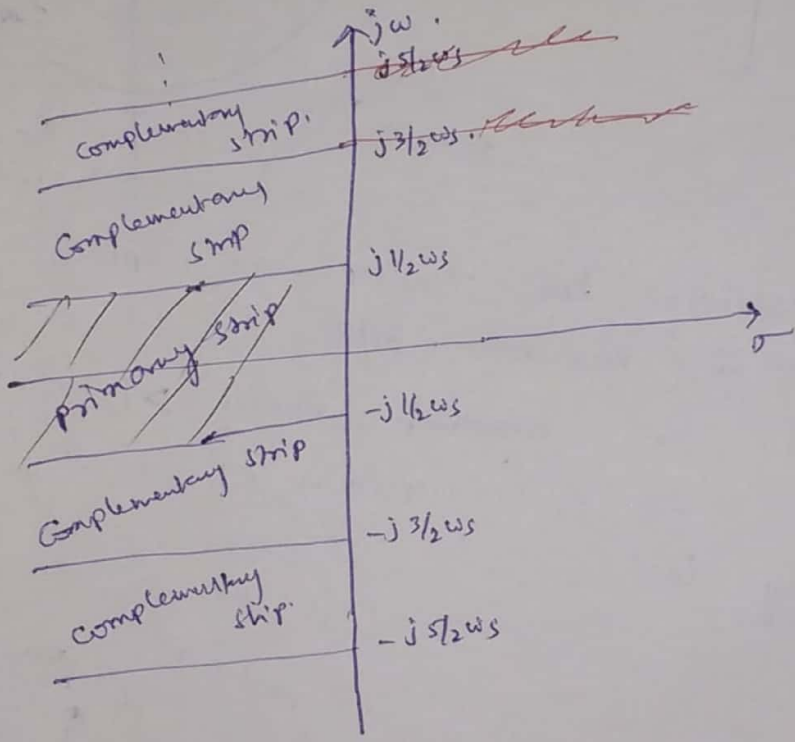
i.e. each strip of width ω_s in the left half of the s -plane maps into the inside of unit circle in the z -plane.

→ i.e. we may divide the left half of s-plane into an infinite number of periodic strips of width ω_s .

$-j\frac{1}{2}\omega_s$ to $j\frac{1}{2}\omega_s \Rightarrow$ Primary strip (maps to a circle)

$j\frac{1}{2}\omega_s$ to $j\frac{3}{2}\omega_s$
 $j\frac{3}{2}\omega_s$ to $j\frac{5}{2}\omega_s$
 \vdots
 $-j\frac{1}{2}\omega_s$ to $-j\frac{3}{2}\omega_s$
 $-j\frac{3}{2}\omega_s$ to $-j\frac{5}{2}\omega_s$
 \vdots

\Rightarrow Complementary strip. (maps on the same circle).



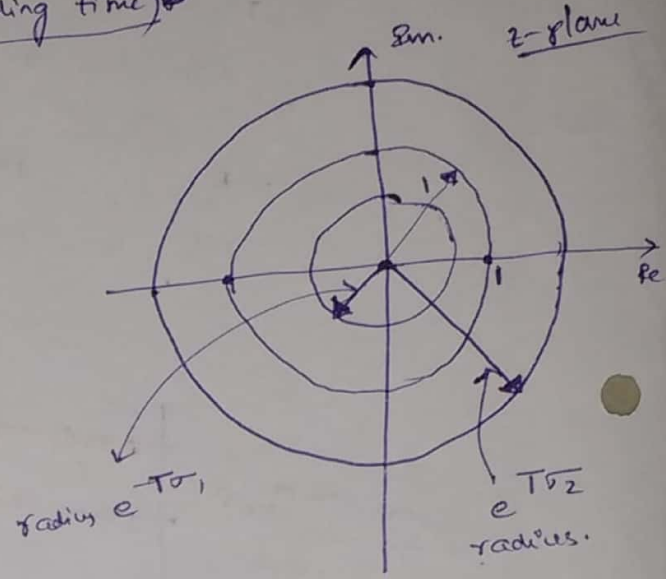
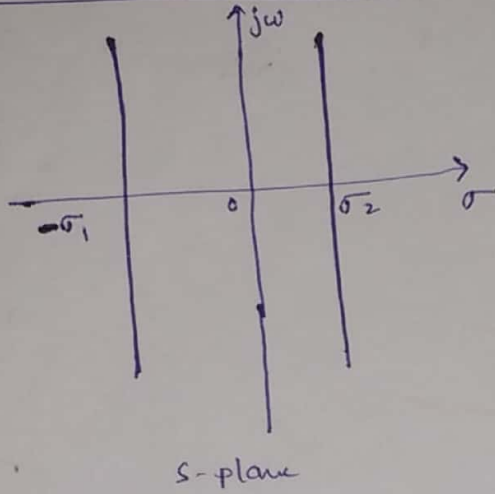
Conclusion

- ① The correspondance between z-plane and s-plane is not unique.
- ② A point in the z-plane corresponds to an infinite number of points in the s-plane.
- ③ But, A point in the s-plane corresponds to a single point in the z-plane.

Mapping of Some Common Contours in s-plane to z-plane:

- ① Constant attenuation loci i.e. $\sigma = \text{constant}$ loci
- ② Constant frequency loci i.e. $\omega = \text{constant}$ loci
- ③ Constant damping loci i.e.

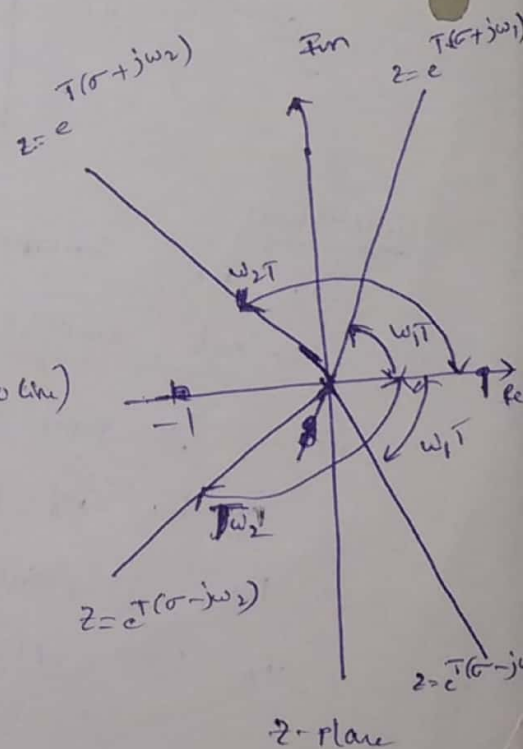
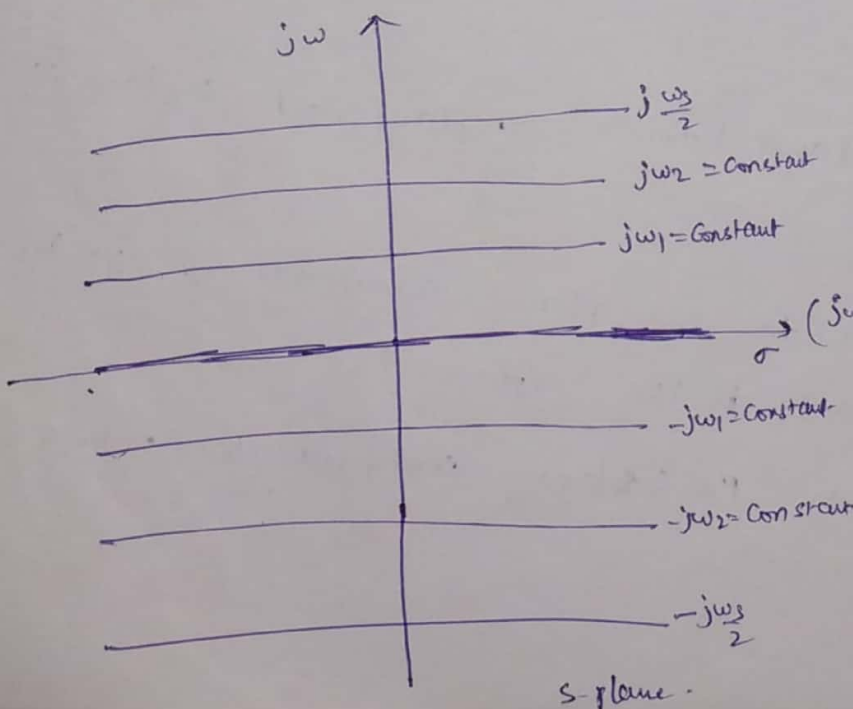
① Constant attenuation loci :- (settling time)



i.e. Constant attenuation ~~loci~~ line in the s-plane maps to a circle of radius $e^{-T\sigma}$.

if $\sigma > 0 \Rightarrow$ ~~radius~~ radius > 1
 if $\sigma < 0 \Rightarrow$ radius < 1 .

② Constant frequency loci :-



$\omega = \pm \frac{1}{2} \omega_s$ line in plane in left half $\xrightarrow{\text{maps}}$

(65) 6.3
negative real axis in the z-plane between 0 & -1

$\omega = \pm \frac{1}{2} \omega_s$ line R.H. plane $\xrightarrow{\text{maps}}$

negative real axis in z-plane between -1 to $-\infty$.

$\omega = \omega_1$ (a constant) line in s-plane $\xrightarrow{\text{maps}}$

a radial line of constant angle $T\omega_1$ (radians) in z-plane.

negative real axis of s-plane $\xrightarrow{\text{maps}}$

positive real axis of z-plane between 0 and 1.

$\omega = \pm n\omega_s$ ($n=0, 1, 2, \dots$) in R.H. plane $\xrightarrow{\text{maps}}$

positive real axis in z-plane between 1 and ∞ .

→ (3) Constant Damping Ratio - ζ axis -

$s = -\zeta \omega_n + j\omega_d$ is the Constant - Damping Ratio line.

$z = e^{Ts} = e^{T[-\zeta \omega_n + j\omega_d]}$

$\omega_d = \omega_n \sqrt{1 - \zeta^2}$
 $T = \frac{2\pi}{\omega_s}$

$= e^{\left[-\frac{2\pi \zeta}{\sqrt{1 - \zeta^2}} \frac{\omega_d}{\omega_s} + j 2\pi \frac{\omega_d}{\omega_s} \right]}$

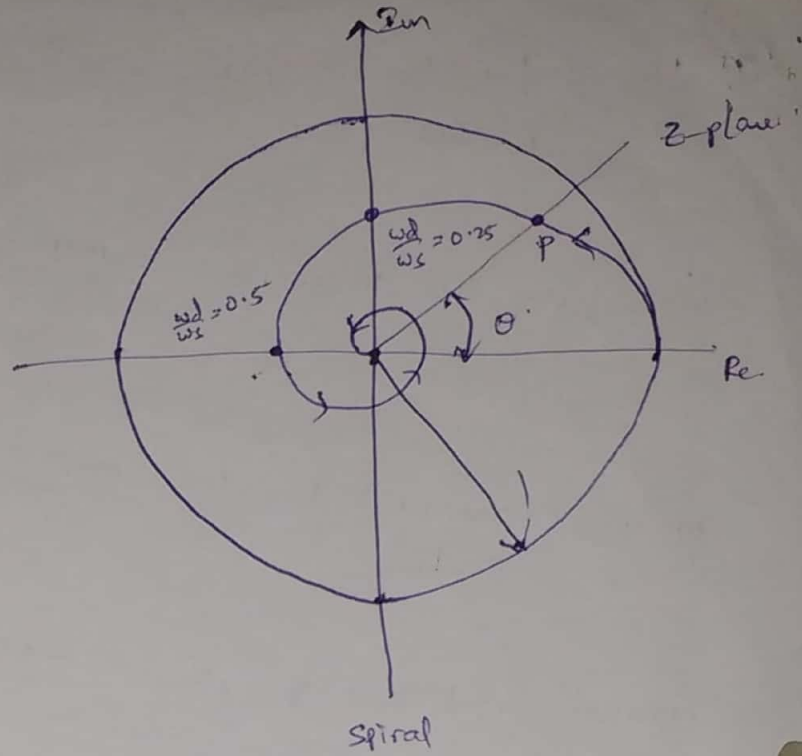
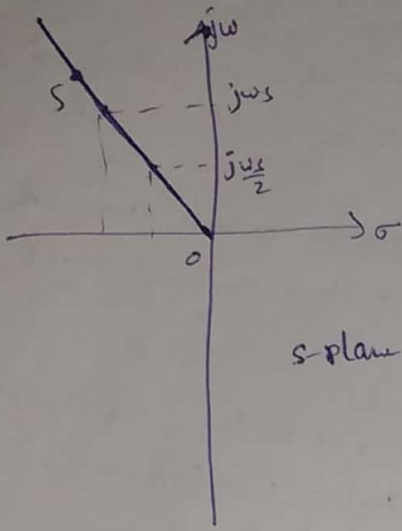
$|z| = e^{\left[\frac{-2\pi \zeta \omega_d}{(\sqrt{1 - \zeta^2}) \omega_s} \right]}$; $\angle z = \frac{2\pi \omega_d}{\omega_s}$

as $\omega_d \uparrow \Rightarrow |z| \downarrow$
 $\omega_s \uparrow \Rightarrow |z| \uparrow$

→ $\frac{\omega_d}{\omega_s}$ is called normalized frequency.

→ if ω_s is given ω_d can be found out at any point on the path.

- draw a line joining origin and p.
- measure the angle w.r.t. to real axis
- then obtain $2\pi \frac{\omega_d}{\omega_s} = \theta$.



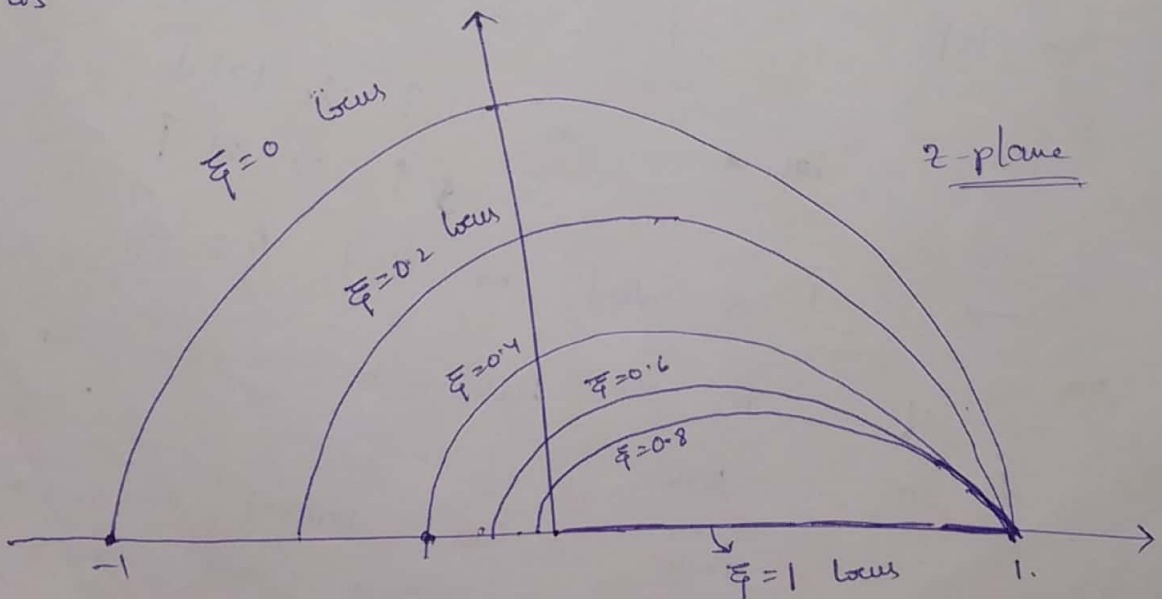
~~if~~ ~~is~~ ~~given~~

Constant damping ratio - line in s-plane

Spiral in z-plane

- ① 2nd (or) 3rd quadrant → Spiral decays within the unit circle.
- ② 1st (or) 4th quadrant → Spiral grows outside the unit circle.

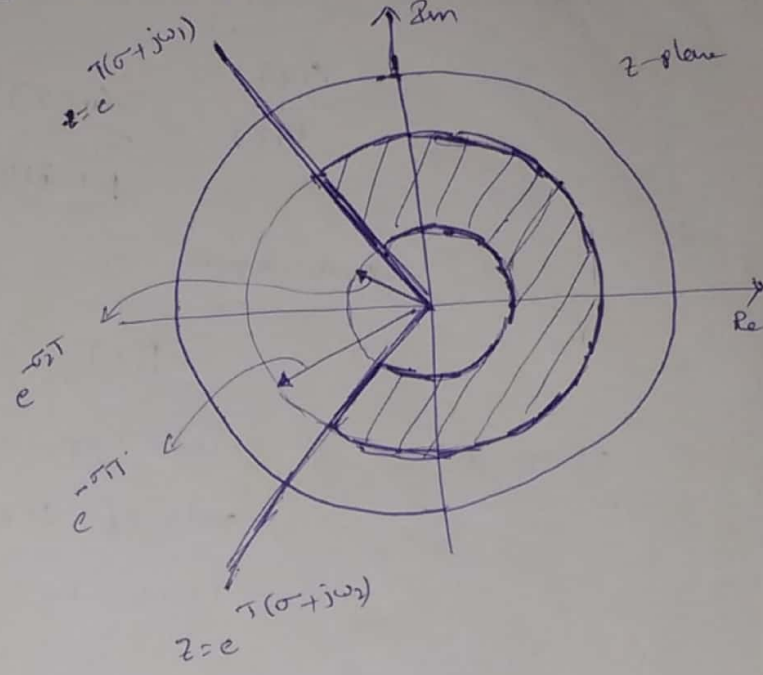
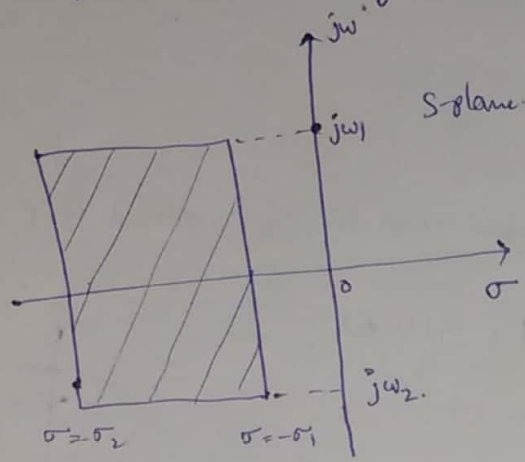
~~if~~ ~~is~~ ~~positive~~



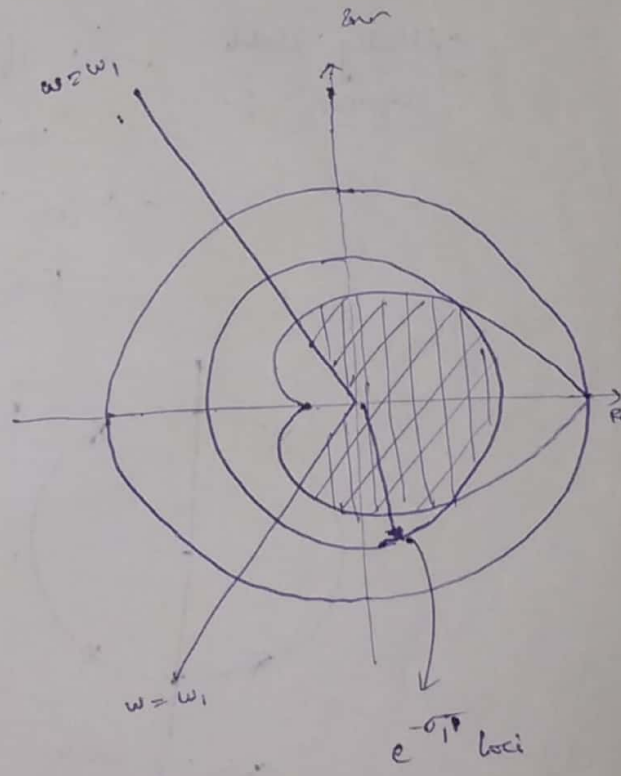
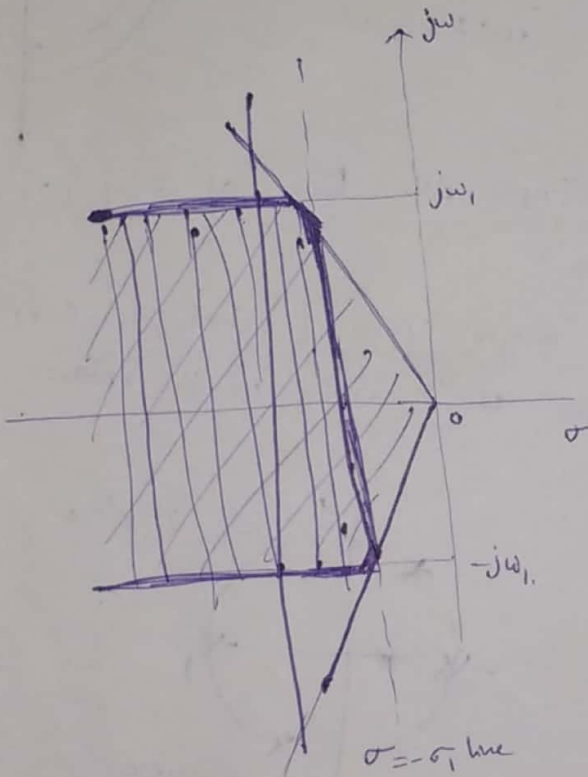
Problems

map the following regions from s-plane to z-plane.

1



2



⇒ Stability Analysis (of L.T.I, SISO, Discrete-Time Control Systems)

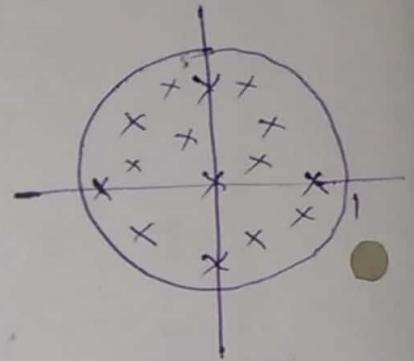
Consider a general closed loop P.T.F

$$C(z) = \frac{G(z)}{1 + GH(z)}$$

The characteristic eqn = denominator of closed loop P.T.F

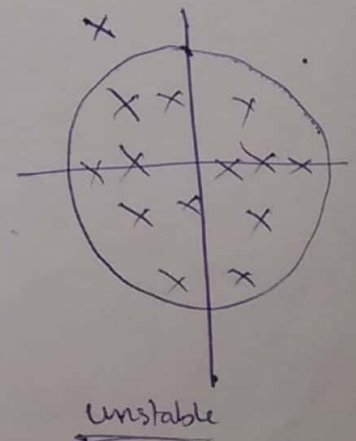
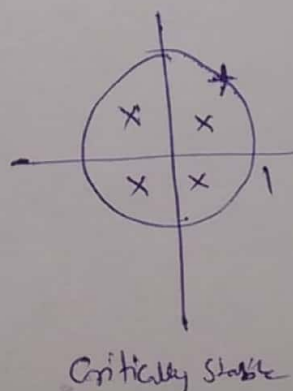
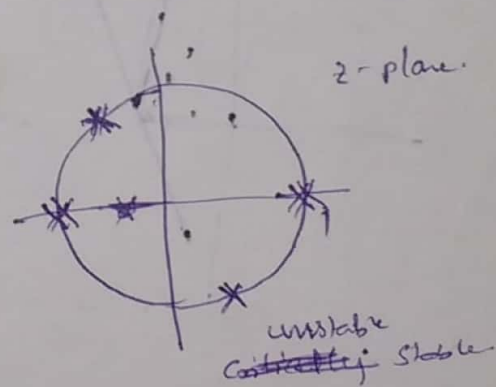
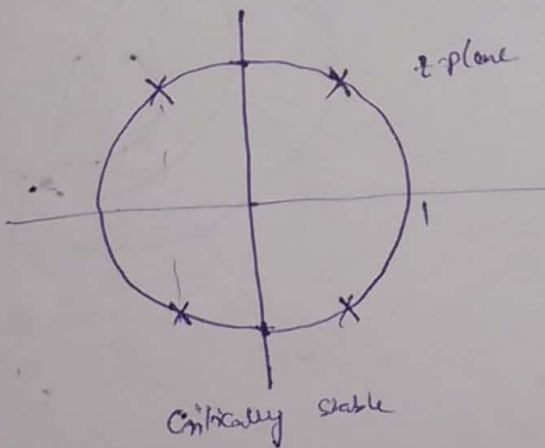
$$P(z) = 1 + GH(z)$$

Stable system → closed loop poles (or) roots of $P(z)$ must lie inside the unit circle



Critically stable system :-

- ① if a simple pole lies at $z=1$ (i.e. on the unit circle)
- ② if a single pair of conjugate complex poles lies on the unit circle in the z-plane.



6

unstable system:-

- ① if roots of $P(z)$ or closed loop poles lie outside the unit circle.
- ② if multiple roots (or multiple closed loop poles) lie on the unit circle.

⇒ Methods for Testing Absolute stability:-

- 1. Jury's stability Test
- 2. Bilinear transformation coupled with Routh stability criterion

① Jury - stability Test

- Gives the existence of any unstable roots (ie roots that lie outside the unit circle.)
- The test neither gives the location of unstable roots nor indicate the effect of parameter changes on the system stability.

→ let $P(z) = a_0 z^n + a_1 z^{n-1} + \dots + a_{n-1} z + a_n$; $a_0 > 0$

Jury table:-

Row	z^0	z^1	z^2	z^3	\dots	z^{n-2}	z^{n-1}	z^n
1	a_n	a_{n-1}	a_{n-2}	a_{n-3}	\dots	a_2	a_1	a_0
2	a_0	a_1	a_2	a_3	\dots	a_{n-2}	a_{n-1}	a_n
3	b_{n-1}	b_{n-2}	b_{n-3}	b_{n-4}	\dots	b_1	b_0	
4	b_0	b_1	b_2	b_3	\dots	b_{n-2}	b_{n-1}	
5	c_{n-2}	c_{n-3}	c_{n-4}	c_{n-5}	\dots	c_0		
6	c_0	c_1	c_2	c_3	\dots	c_{n-2}		
\vdots	\vdots							
$2n-5$	p_3	p_2	p_1	p_0				
$2n-4$	p_0	p_1	p_2	p_3				
$2n-3$	q_2	q_1	q_0					

$$b_k = \begin{vmatrix} a_n & a_{n-1-k} \\ a_0 & a_{k+1} \end{vmatrix} \quad k = 0, 1, 2, \dots, n-1$$

$$c_k = \begin{vmatrix} b_{n-1} & b_{n-2-k} \\ b_0 & b_{k+1} \end{vmatrix} \quad k = 0, 1, 2, \dots, n-2$$

$$q_k = \begin{vmatrix} p_3 & p_{2-k} \\ p_0 & p_{k+1} \end{vmatrix} \quad k = 0, 1, 2$$

Condition for stability :-

1. $|a_n| < a_0$;
2. $P(z) \big|_{z=1} > 0$
3. $P(z) \big|_{z=-1} \begin{cases} > 0 & \text{for } n \text{ even} \\ < 0 & \text{for } n \text{ odd.} \end{cases}$
4. $|b_{n-1}| > |b_0|$
5. $|c_{n-2}| > |c_0|$
6. $|q_2| > q_0$

for a 4th order polynomial :- $f(z) = a_0 z^4 + a_1 z^3 + a_2 z^2 + a_3 z + a_4$.

$$b_3 = \begin{vmatrix} a_4 & a_0 \\ a_0 & a_4 \end{vmatrix} ; b_2 = \begin{vmatrix} a_4 & a_1 \\ a_0 & a_3 \end{vmatrix} ; b_1 = \begin{vmatrix} a_4 & a_2 \\ a_0 & a_2 \end{vmatrix} ; b_0 = \begin{vmatrix} a_4 & a_3 \\ a_0 & a_1 \end{vmatrix}$$

$$c_2 = \begin{vmatrix} b_3 & b_0 \\ b_0 & b_3 \end{vmatrix} ; c_1 = \begin{vmatrix} b_3 & b_1 \\ b_0 & b_2 \end{vmatrix} ; c_0 = \begin{vmatrix} b_3 & b_2 \\ b_0 & b_1 \end{vmatrix}$$

array :-

rows	z^0	z^1	z^2	z^3	z^4
1	a_4	a_3	a_2	a_1	a_0
2	a_0	a_1	a_2	a_3	a_4
3	b_3	b_2	b_1	b_0	
4	b_0	b_1	b_2	b_3	
$(2n-3)$ 5	c_2	c_1	c_0		

for a 3rd-order Polynomial.

(6.6)

6.6

$$P(z) = a_0 z^3 + a_1 z^2 + a_2 z + a_3$$

	z^0	z^1	z^2	z^3
1	a_3	a_2	a_1	a_0
2	a_0	a_1	a_2	a_3
$(2n-3) = 3$	b_2	b_1	b_0	

$$b_2 = \begin{vmatrix} a_3 & a_0 \\ a_0 & a_3 \end{vmatrix}; \quad b_1 = \begin{vmatrix} a_3 & a_1 \\ a_0 & a_2 \end{vmatrix}; \quad b_0 = \begin{vmatrix} a_3 & a_2 \\ a_0 & a_1 \end{vmatrix}$$

Ex Consider the D.T unity-feedback control system (with $T=1$), whose open-loop P.T.F is

$$G(z) = \frac{k(0.3679z + 0.2642)}{(z - 0.3679)(z - 1)}$$

Determine the range of k for stability by use of Jury stability Test

Sol

$$\text{C.L. P.T.F} = \frac{G(z)}{1+G(z)} = \frac{k(0.3679z + 0.2642)}{z^2 + (0.3679k - 1.3679)z + 0.3679 + 0.2642k}$$

order of the polynomial $P(z) = z^2 + (0.3679k - 1.3679)z + 0.3679 + 0.2642k$.

$$\text{order} = 2$$

$$\therefore \text{No. of rows} = (2n-3) = \underline{1}$$

\therefore array

	z^2	z^1	z^0
	a_2	a_1	a_0

where

$$a_0 = 1$$

$$a_2 = 0.3679 + 0.2642k$$

For a stable system according to Jury stability

① $|a_2| < a_0$

② $P(1) > 0$

③ $P(-1) > 0$ ($\because n=2$ even number)


① $\Rightarrow |0.3679 + 0.2642k| < 1 \Rightarrow$



$\Rightarrow (0.3679 + 0.2642k) < 1 \Rightarrow k < 2.3925$; $-(0.3679 + 0.2642k) < -1 \Rightarrow k > -5.177$

② $\Rightarrow P(1) = 1 + (0.3679k - 1.3679) + 0.3679 + 0.2642k > 0$
 $\therefore k > 0$

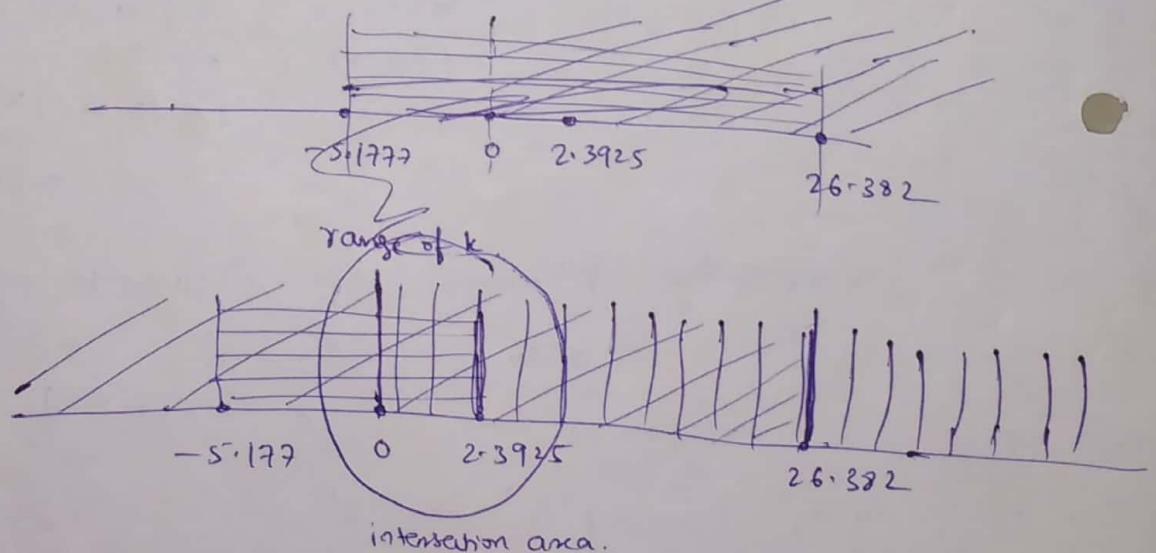
③ $\Rightarrow P(-1) = 1 - (0.3679k - 1.3679) + 0.3679 + 0.2642k > 0$
 $= 26.382 > k$

\therefore k value must satisfy

① $\Rightarrow 2.3925 > k > -5.1777$ 

② $\Rightarrow k > 0$  

③ $\Rightarrow k < 26.382$ 



\therefore k range is $0 < k < 2.3925$.

or $k \in (0, 2.3925)$

Ex 6.7 using Jury stability Test obtain the stability of the following Discrete time systems. (6.7)

(i) $z^3 + 3.3z^2 + 4z + 0.8 = 0$ (ii) $z^3 - 1.1z^2 - 0.1z + 0.2 = 0$

sol (i)

$P(z) = z^3 + 3.3z^2 + 4z + 0.8$

Comparing w $P(z) = a_0 z^3 + a_1 z^2 + a_2 z + a_3$

$a_3 = 0.8 \quad a_2 = 4 \quad a_1 = 3.3 \quad a_0 = 1$

Order of polynomial = $n = 3$.

\therefore no. of rows = $2n - 3 = 3$.

	z^0	z^1	z^2	z^3
1	0.8	4	3.3	1
2	1	3.3	4	0.8
3	-0.36	-0.1	-1.36	

$b_2 = -0.36$

$b_1 = -0.1$

$b_0 = -1.36$

Jury stability Test

(1) $|a_n| < a_0$ i.e. $a_3 < a_0$ satisfied.

(2) $P(1) > 0 \Rightarrow 1 + 3.3 + 4 + 0.8 > 0$ satisfied.

(3) $P(-1) < 0 \Rightarrow -1 + 3.3 - 4 + 0.8 < 0$ satisfied.
($\because n = 3$ odd)

(4) $|b_2| > |b_0|$ not satisfied.

\therefore system is unstable.

Ex 7 examine the stability of the following characteristic equation.

$P(z) = z^4 - 1.2z^3 + 0.07z^2 + 0.3z - 0.08$

$(z - 0.8)(z - 0.5)(z - 0.5)(z - 0.4) = 0$

P2

Consider the following .

$$y(k) - 0.6y(k-1) + 0.81y(k-2) - 0.67y(k-3) + 0.12y(k-4) = x(k)$$

Determine the stability .

sol

applying z-transform.

$$Y(z) - 0.6z^{-1}Y(z) + 0.81z^{-2}Y(z) - 0.67z^{-3}Y(z) + 0.12z^{-4}Y(z) = X(z)$$

$$\frac{Y(z)}{X(z)} = \frac{1}{1 - 0.6z^{-1} + 0.81z^{-2} - 0.67z^{-3} + 0.12z^{-4}}$$

$$= \frac{z^4}{z^4 - 0.6z^3 + 0.81z^2 - 0.67z + 0.12}$$

Comparing $a_0 = 1$ $a_1 = -0.6$ $a_2 = -0.81$ $a_3 = 0.67$ $a_4 = -0.12$

order of the system = $n = 4$.

\therefore no. of rows = $2n - 3 = 5$.

	z^0	z^1	z^2	z^3	z^4
1	a_4 -0.12	a_3 0.67	a_2 -0.81	a_1 -0.6	a_0 1
2	a_0 1	a_1 -0.6	a_2 -0.81	a_3 0.67	a_4 -0.12
3	b_3 -0.9856	b_2 0.5196	b_1 0.9072	b_0 -0.5980	
4	b_0 -0.5980	b_1 0.9072	b_2 0.5196	b_3 -0.9856	
5	c_2 0.6138	c_1 0.033	c_0 -0.5834		

Test

① $|a_4| < a_0$ Satisfied.

② $P(1) \Rightarrow 1 - 0.6 - 0.81 + 0.67 - 0.12 = 0.14 > 0$ Satisfied.

③ $P(-1) \Rightarrow 1 + 0.6 - 0.81 - 0.67 - 0.12 = 0$

i.e. there is a root $z = -1$.

④ $|b_3| > |b_0|$ Satisfied.

⑤ $|c_2| > |c_0|$ Satisfied.

\therefore critically stable.

⇒ stability analysis using Bilinear - transformation (20) (6.8)

Coupled with Routh's stability criterion

→ This method Requires transformation from z-plane to other complex plane, ~~called~~ say w-plane.

→ The bilinear - transformation is defined by

$$z = \frac{w+1}{w-1} \Rightarrow w = \frac{z+1}{z-1}$$

mapping between z-plane & w-plane.

in z-plane \longleftrightarrow in w-plane

Inside the unit circle \longrightarrow left half of w-plane.

unit circle \longrightarrow imaginary axis of w-plane

Outside the unit circle \longrightarrow Right half of w-plane

steps

1. Substitute $\frac{w+1}{w-1}$ in place of z in the characteristic eqn.

then $P(z) \Rightarrow a_0 z^n + a_1 z^{n-1} + \dots + a_{n-1} z + a_n = 0$ becomes

$$Q(w) \Rightarrow a_0 \left(\frac{w+1}{w-1}\right)^n + a_1 \left(\frac{w+1}{w-1}\right)^{n-1} + \dots + a_{n-1} \left(\frac{w+1}{w-1}\right) + a_n = 0$$

2. clear the fractions ~~now~~ by multiplying the above $Q(w)$ both sides with $(w-1)^n$. then we obtain

$$Q(w) = b_0 w^n + b_1 w^{n-1} + \dots + b_{n-1} w + b_n = 0$$

3. Apply the Routh stability criterion in the same manner as in Continuous - time systems.

⇒ Composition between Jury stability and stability by

Bilinear-transformation :-

- ① Computationally Jury stability test is simpler.
- ② The no. of poles inside the unit circle, on the unit circle and outside the unit circle can't be found by Jury stability criterion whereas it is possible by Bilinear-transformation.

Q20
Given $P(z) \Rightarrow z^3 - 1.3z^2 - 0.08z + 0.24 = 0$. we

Bilinear transformation for stability.

Q21
1. $\left(\frac{w+1}{w-1}\right)^3 - 1.3\left(\frac{w+1}{w-1}\right)^2 - 0.08\left(\frac{w+1}{w-1}\right) + 0.24 = 0$

2. multiply with $(w-1)^3$.

$$(w+1)^3 - (1.3)(w+1)^2(w-1) - 0.08(w+1)(w-1)^2 + 0.24(w-1)^3 = 0$$

$$w^3 + 1 + 3w^2 + 3w - 1.3[w^3 + w + 2w^2 - w^2 - 1 - 2w] - 0.08[w^3 + w - 2w^2 + w^2 + 1 - 2w] + 0.24[w^3 - 1 - 3w^2 + 3w] = 0$$

$$\therefore Q(w) \Rightarrow -0.14w^3 + 1.06w^2 + 5.10w + 1.98 = 0$$

$$\Rightarrow w^3 - 7.571w^2 - 36.43w - 14.14 = 0$$

Routh's criterion :-

↗	w^3	1	-36.43
↘	w^2	-7.571	-14.14
	w^1	-38.3	0
	w^0	-14.14	

one root \rightarrow R.H of w -plane \Rightarrow outside the unit circle.

\therefore unstable.

Q2 $4z^3 - 4z^2 - 7z - 2 = 0$